

Multistage Rate Change

Motivation for Multi-Stage Schemes

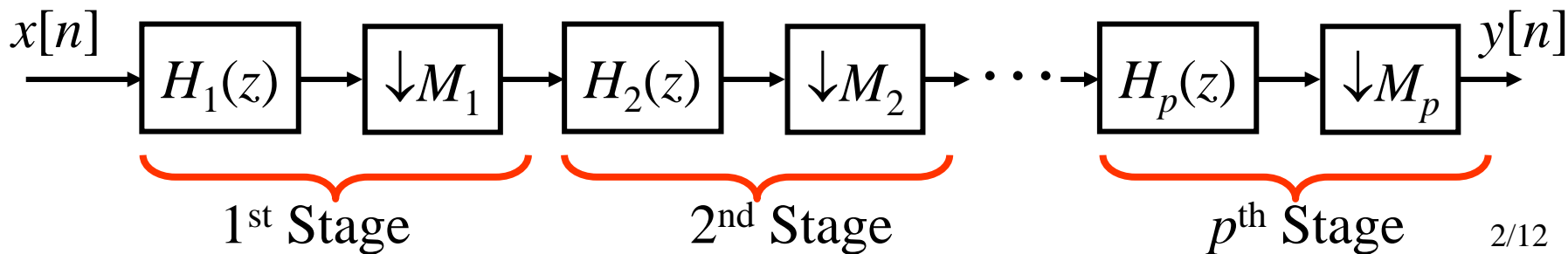
Consider Decimation:

When M is large (typically > 10 or so) it is usually inefficient to implement decimation in a single step (i.e., in a single stage).

The Culprit: Large M requires the LPF to have a stopband edge of $\theta_s = \pi/M$, which is small for large M

- Need a LPF with a very narrow passband
- Requires a long FIR filter
- Inefficient since long filters require a large # of multiplies

Solution: If M can be factored into a product of integers ($M = M_1 M_2 M_3 \dots M_p$). Then decimation by M can be done by:



Trick to Get Efficiency from Multi-Stage

The design of $H_1(z)$ (& other “front-end” stages) can be relaxed from what you would use for a single-stage design.

Certainly, you need $H_1(z)$ to have $\theta_s = \pi/M_1 > \pi/M$ so no aliasing occurs after $\downarrow M_1 \dots$

But... it is even better than that.

Can let $\theta_s > \pi/M_1 \dots$ which lets some aliasing occur

But... only so much aliasing – such that the aliasing that occurs gets suppressed by the next filter, $H_2(z)$

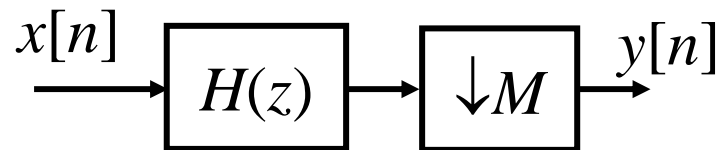
Higher Stopband Edge \rightarrow Shorter Filter \rightarrow More Efficient

Let's See Why for a 2-Stage Case

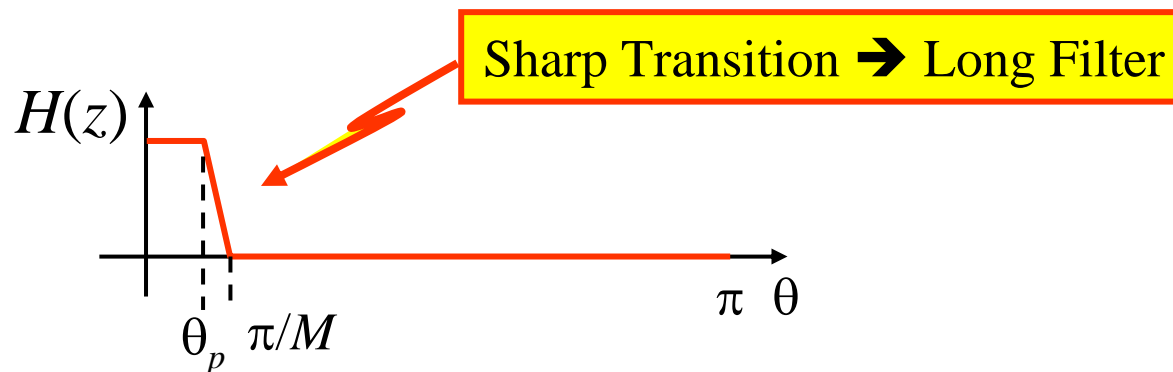
Say that the signal $x[n]$ has “spectral content of worth” only up to frequency $\theta = \theta_p < \pi/M \dots$ with $M = M_1 M_2$.

Single-Stage Method

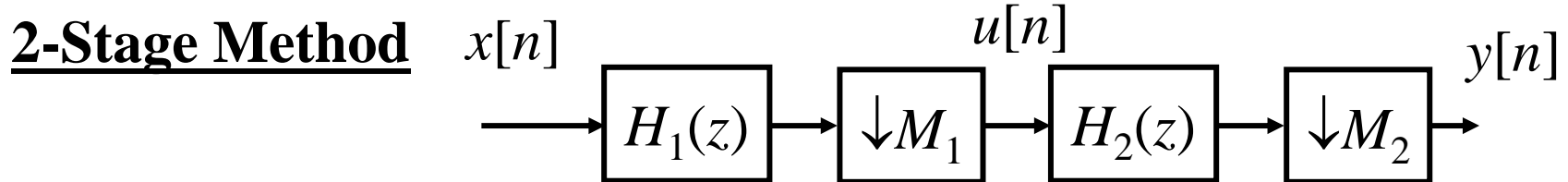
Suppose we decimate using a single-stage scheme:



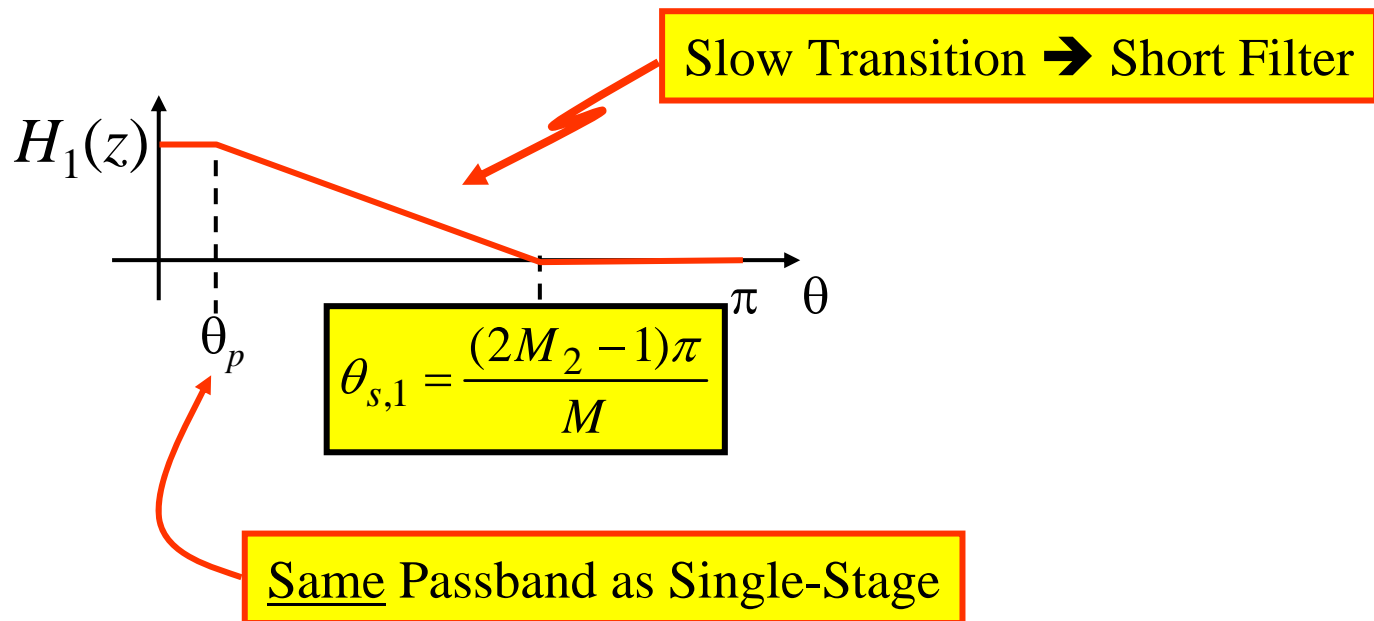
Then we need



Let's See Why for a 2-Stage Case (cont.)



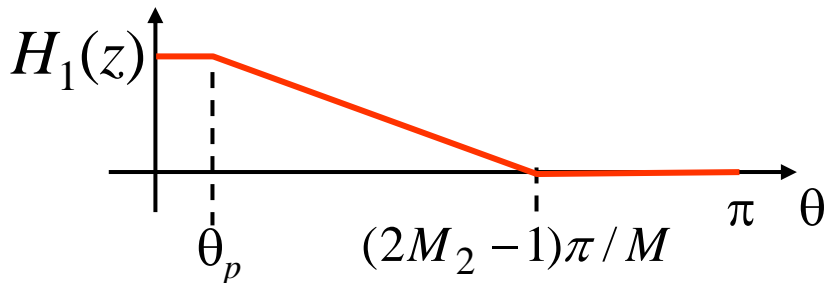
After $H_1(z)$ but before $\downarrow M_1$ we need:



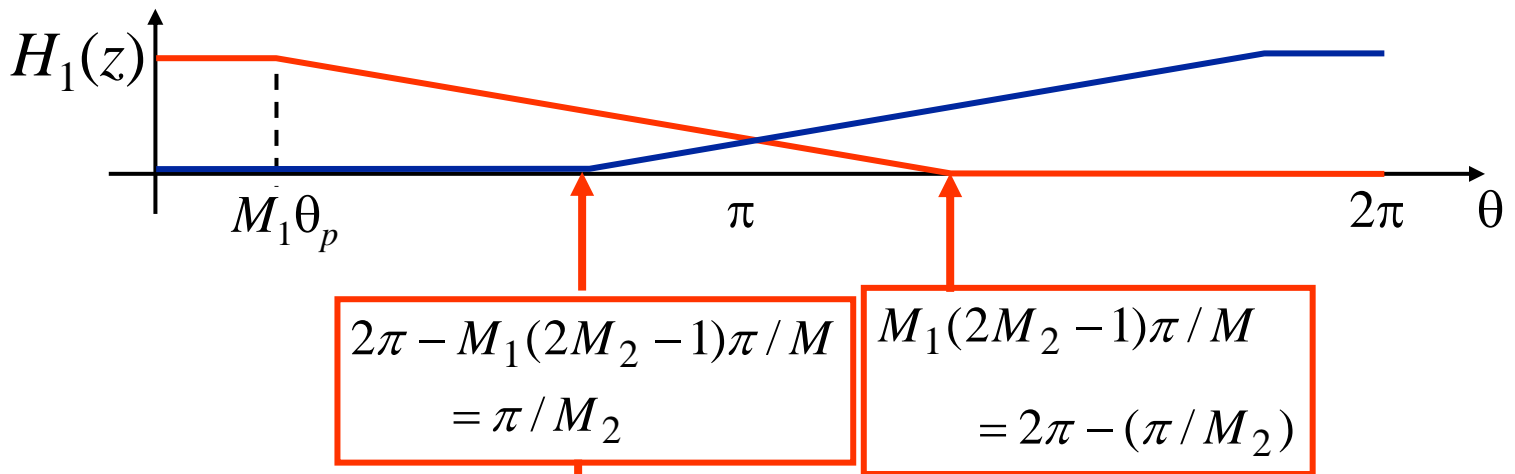
Let's See Why for a 2-Stage Case (cont.)

Let's see the impact of this slower transition on aliasing:

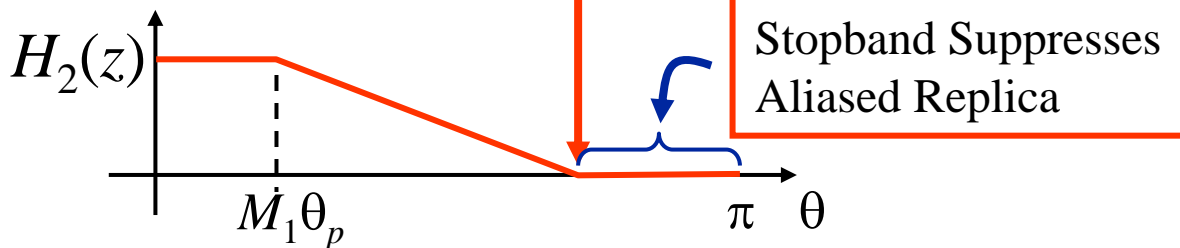
After
1st
Filter



After
1st
Dec



After
2nd
Filter



Design Requirements

So... say you want to design a 2-stage multirate scheme instead of a 1-stage multirate scheme:

If single stage, say the specs need to be:

- Passband Cutoff = θ_p
- Stopband Cutoff = θ_s
- Passband Ripple = δ_p
- Stopband Level = δ_s

For a 2-stage scheme, our above results say we need:

• 1st Stage

- $\theta_{p,1} = \theta_p$
- $\theta_{s,1} = (2M_2 - 1)\pi/M > \theta_s$
- $\delta_{p,1} = \delta_p/2$
- $\delta_{s,1} = \delta_s$

• 2nd Stage

- $\theta_{p,2} = M_1\theta_p$
- $\theta_{s,2} = \pi/M_2$
- $\delta_{p,2} = \delta_p/2$
- $\delta_{s,2} = \delta_s$

Passband Ripple is split between 2 filters

Example: How 2-Stage Reduces Computation

Goal: Decimation by $M = 12$

Filter Requirements

$\delta_p = 0.01$ ← to give some desired fidelity (application specific)

$\delta_s = 0.001$ ← to limit aliasing to desired level (application specific)

$\theta_p = \pi/16$ ← to pass desired band (application specific)

$\theta_s = \pi/12 = \pi/M$ ← to prevent aliasing for desired decimation rate

Single-Stage Method

Length of filter determines the # of computations

→ Use (10.2.94) in P&M to estimate filter order needed:

$$N = \frac{-20 \log_{10} \sqrt{\delta_p \delta_s} - 13}{2.32 \underbrace{|\theta_s - \theta_p|}_{\substack{\text{transition} \\ \text{width}}}}$$

Example: Single-Stage Method (cont.)

Using this order estimate for the given filter requirements gives:

$$N = 244 \rightarrow \text{Length: } L = N + 1 = 245$$

Note: #'s given below differ slightly from book because it (wrongly) uses N instead of L in its computation estimates

Our chosen complexity measure: # Multiplies/Input Sample

Each output sample (after decimation): **L Multiplies/Output Sample**

There are **M Input Samples/Output Sample** (due to decimation)

$$\rightarrow (\# \text{ Multiplies}) / (\text{Input Sample}) = \frac{L \text{ mult/output}}{M \text{ input/output}} = \frac{L}{M} = \frac{245}{12} \approx 20.4$$

Single-Stage Complexity = 20.4 multiplies/input

Ex. Cont.: Double-Stage Method ($M = M_1 M_2: 12 = 3 \times 4$)

1st Stage

- $\theta_{p,1} = \theta_p = \pi/16$ $\delta_{p,1} = \delta_p/2 = 0.005$
- $\theta_{s,1} = (2M_2-1)\pi/M = 7\pi/12$ $\delta_{s,1} = \delta_s = 0.001$

Estimated filter order gives: $\rightarrow N_1 = 11$ $\rightarrow L_1 = 12$

So... Mult/Input = $L_1/M_1 = 12/3 = 4$

2nd Stage

- $\theta_{p,2} = M_1 \theta_p = 3\pi/16$ $\delta_{p,2} = \delta_p/2 = 0.005$
- $\theta_{s,2} = \pi/M_2 = \pi/4$ $\delta_{s,2} = \delta_s = 0.001$

Estimated filter order gives: $\rightarrow N_2 = 88$ $\rightarrow L_2 = 89$

So... Mult/Input = $L_2/(M_1 M_2) = 89/12 = 7.4$

referenced back to input of whole system

Double-Stage Complexity = $4 + 7.4 = 11.4$ multiplies/input
2-Stage has $\approx 1/2$ Complexity of 1-Stage

Comments on Multistage Method

Q: What happens in this example when order of stages is switched?
i.e., $M_1 = 4$ and $M_2 = 3$ (Left as Exercise!!!)

These 2-Stage design ideas can be extended to p-stage designs:

$$M = M_1 M_2 M_3 \dots M_p$$

The order of these multiple stages matters

Similar ideas can be used for multistage interpolation

Application: Multistage Rate Change

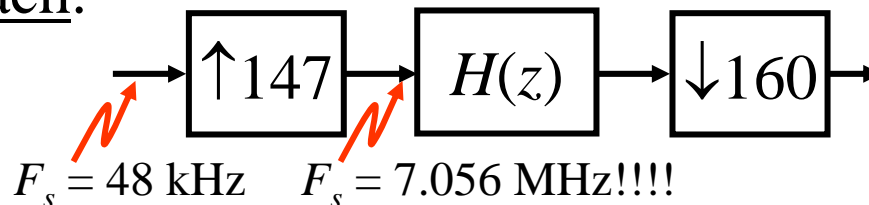
Convert Digital Audio Tape (DAT) format to Compact Disk (CD)

DAT uses $F_s = 48 \text{ kHz}$ CD uses $F_s = 44.1 \text{ kHz}$	→	$\frac{44.1 \times 10^3}{48 \times 10^3} = \frac{441}{480} = \frac{3 \times 147}{3 \times 160} = \frac{147}{160}$
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→

$\text{Rate Change Ratio} = \frac{L}{M} = \frac{147}{160}$
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Single-Stage Approach:



Multiple-Stage Approach:

$$L = 147 = 7 \times 7 \times 3$$

$$M = 160 = 5 \times 8 \times 4$$

